



An Effective Technique for Diminution of Inrush Current of Load Transformers for Voltage Sag Compensator

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ABSTRACT

Power quality issues have gotten much consideration as of late. In numerous nations, cutting edge producers gather in industry parks. Along these lines, any power quality occasions in the utility network can influence countless makers. Overview results recommend that 92% of intrusion at modern offices is voltage list related. In this project, the inrush issue of burden transformers under the task of the hang compensator is displayed. An inrush moderation method is proposed and actualized in a synchronous reference edge hang compensator controller. The voltage hang compensator comprises of a three stage voltage source inverter (VSI) and a coupling transformer for sequential association. The voltage hang compensator, in view of a transformer-coupled arrangement associated voltage source inverter, is among the most financially savvy arrangement against voltage lists. Transformers are frequently introduced before basic burdens for electrical detachment purposes. At the point when voltage hangs occur, the transformers are presented to the distorted voltages and a DC counterbalance will happen in its transition linkage. At the point when the compensator reestablishes the heap voltage, the transition linkage will be headed to the dimension of attractive immersion and serious inrush current

happens. The motion linkage is evaluated by the deliberate line voltage. What's more, this method can be flawlessly coordinated with the state criticism controller of the compensator. The controller incorporates a voltage control, a present control and a motion linkage control. This control strategy is additionally founded on the synchronous reference outline which empowers voltage droop compensator to accomplish quick voltage infusion and anticipate the inrush current. The synchronous reference outline execution of the proposed state input controller can viably improve the unsettling influence dismissal ability contrasted with the stationary edge criticism controller structure. At the point when voltage droop happens, the controller can follow the transient motion linkage and ascertain a required pay voltage continuously for quick pay and end of transition linkage DC counterbalance brought about by voltage hangs. The proposed technique can be effectively coordinated with the current voltage droop remuneration control framework without utilizing any additional sensors.

Keywords :— Voltage sags, Utility systems, Voltage source converters, Inrush Current Mitigation Technique

I. INTRODUCTION

Power quality issues have received much consideration as of late. In numerous nations, cutting edge makers move in industry parks. Along these lines, any power quality occasions in the utility network can influence an enormous number of producers. Records demonstrate that voltage droop, homeless people and flashing interference comprise 92% of the power quality issues. The voltage list implies that the root mean square estimation of basic voltage incidentally decreases to 0.1~0.9 per unit and keeps up 0.5 to 30 cycle. Voltage droops regularly intrude on basic loads and results in considerable profitability misfortunes. Voltage hang compensators have been a standout amongst the most financially savvy voltage droop ride through arrangements. A few shut circle control strategies have been proposed for voltage source inverter-based list compensators. In this paper, the inrush issue of burden transformers under the activity of the hang compensator is displayed. An inrush alleviation system is proposed and actualized in a synchronous reference casing droop compensator controller. The proposed system can be coordinated with the traditional shut circle control on burden voltages. The new coordinated control can effectively lessen inrush current of burden transformers, and improve the unsettling influence dismissal capacity and the strength of the list compensator framework. Lab test outcomes are exhibited to approve the proposed strategy. The voltage droop compensator comprises of a three stage voltage source inverter (VSI) and a coupling transformer for sequential association. At the point when the framework is ordinary, the compensator is circumvent by the thyristors for high working productivity. At the point when voltage droops happen, the voltage list

compensator infuses the required remuneration voltage through the coupling transformer to shield touchy burdens from being hindered by lists. Nonetheless, certain recognition time (commonly inside 4ms) is required by the droop compensator controller to distinguish the hang even. What's more, the heap transformer is presented to the disfigured voltage from the droop event to the minute when the compensator reestablishes the heap voltage. But its brief span, the distorted voltage causes attractive transition linkage deviation inside the heap transformer, and attractive immersion may effectively happen when the compensator reestablishes the heap voltage, hence results in inrush current. The inrush current could trigger the over-current assurance of the compensator and lead to pay disappointment. Along these lines this paper proposes inrush relief method by revising the transition linkage balances of the heap transformer. What's more, this procedure can be consistently incorporated with the state criticism controller of the compensator.

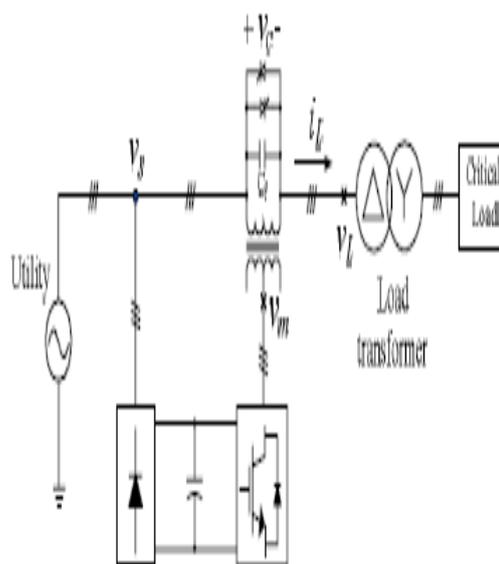


Figure 1 : A simplified one-line diagram of the off-line series voltage sag compensator

II. POWER QUALITY

The contemporary compartment crane industry, in the same way as other industry sections, is regularly fascinated by the fancy odds and ends, bright symptomatic presentations, fast execution, and dimensions of computerization that can be accomplished. In spite of the fact that these highlights and their in a roundabout way related PC based upgrades are key issues to an effective terminal activity, we should not overlook the establishment whereupon we are building. Power quality is the mortar which bonds the establishment squares. Power quality additionally influences terminal working financial aspects, crane dependability, our condition, and introductory interest in power circulation frameworks to help new crane establishments. To cite the service organization pamphlet which went with the last month to month issue of my home utility charging: 'Utilizing power admirably is a decent ecological and business practice which sets aside you cash, diminishes emanations from producing plants, and moderates our normal assets.' As we are for the most part mindful, holder crane execution necessities keep on expanding at a shocking rate. Cutting edge holder cranes, as of now in the offering procedure, will require normal power requests of 1500 to 2000 kW – practically twofold the absolute normal interest three years prior. The quick increment in power request levels, an expansion in compartment crane populace, SCR converter crane drive retrofits and the enormous AC and DC drives expected to power and control these cranes will expand consciousness of the power quality issue in the exceptionally not so distant future.

III. VOLTAGE SAGS

A decrease in voltage enduring any place from milliseconds up to a couple of

moments. Hangs keep a machine from the power it needs to work, causing PC accidents or gear lock-ups. Typically brought about by hardware start-up, for example, lifts, warming and cooling gear, blowers, and copiers—or close-by short circuits on the utility framework. The estimation of a Voltage Sag is expressed as a level of the ostensible voltage it is an estimation of the rest of the voltage and is expressed as list to a rate esteem. Along these lines a Voltage Sag to 60% is equal to 60% of ostensible voltage, or 288 Volts for an ostensible 480 Volt framework.

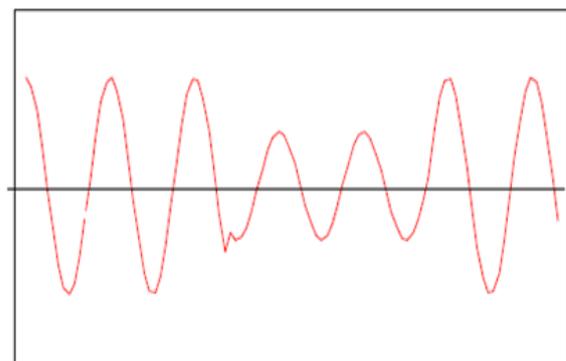


Figure 2 : Voltage Sag- A Reduced Voltage for a Limited Periodic

Voltage hangs are presumably the most huge power quality (PQ) issue confronting modern clients today, and they can be a noteworthy issue for huge business clients too. There are two wellsprings of voltage droops: outside (on the utility's lines up to your office) and inward (inside your office). Utilities persistently endeavor to give the most dependable and steady electric power conceivable. Over the span of typical utility tasks, in any case, numerous things can cause voltage hangs. Tempests are the most widely recognized reason for outside droops and flitting intrusions in many regions of the U.S.A tempest going through a zone can result in many major and minor PQ varieties, including droops. For instance, think about how PQ would be influenced by a lightning

strike on or close to an electrical cable or by wind sending tree appendages into electrical cables. Other regular reasons for outside voltage hangs are ice storms, creatures (especially squirrels), and the start-up of huge burdens at neighboring offices. Inner reasons for voltage droops can incorporate beginning real loads and establishing or wiring issues. Demonstrates a case of hang on a three stage circuit, checked by PTs with a 120 volt ostensible yield. The list started on Phase An, and included Phase B3 cycles later. Various understood examinations have been led in the past concerning recurrence and degree of intensity quality unsettling influences. Two ongoing investigations have been led by the Electric Power Research Institute (EPRI) and the National Power Laboratories (NPL) on the appropriation and purpose of-utilization levels, individually. The EPRI supported program has utilized 300 power quality observing hubs on the conveyance frameworks of 24 utilities through US, which was attempted by Electro tek Concepts, Inc. Checking units, were put at the conveyance substation, at a point close to the center of the feeder, and at a point close to the finish of the feeder. It has been accounted for that roughly 42% of the hangs saw to date were outside CBEMA limits.

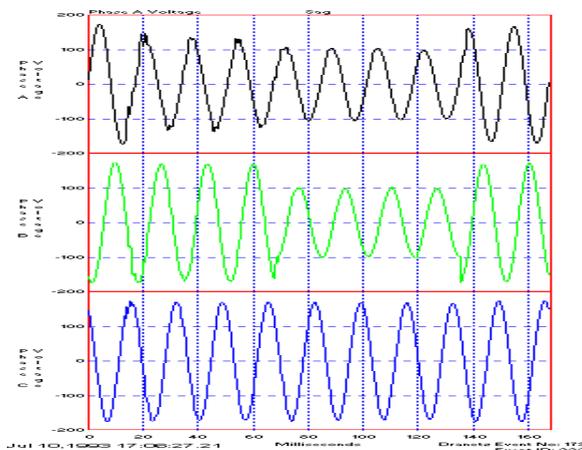


Figure 3: Different Phase Voltage Sags for 3Phase System

Figure 3 demonstrates a chart of the dispersion by span of hangs underneath 90 Vrms. The NPL study was a multi year consider somewhere in the range of 1990 and 1994 of purpose of-usage control quality checking at 112 North American areas. Single stage, line-toneutral information was gathered at the standard divider repository. Screens were set for differing time allotments at the site, contingent upon the need to decide climatic impacts and other corresponding variables. Destinations included: a climactic and geographic cross segment of the US, cross segment of significant sorts of utility burdens (overwhelming industry, light industry, office and retail locations, private, blended); and, an expansive scope of structure areas, building types, building ages, and populace zones. A 104 Vrms limit for list and 127 Vrms limit for a swell was utilized, according to the ANSI C84.1-1989 points of confinement and CBEMA bend. An amount of 1057 site a very long time of information was gathered, which yielded more than 160,000 power unsettling influences amid the observing time frame. Hangs were the most common sort of occasions, averaging 27.9 every month, with normal list abundance of 99.3 Vrms. The middle length of list was 0.26 sec, versus a 2.1 sec normal, which the consequence of a few long haul droops.

IV. VOLTAGE SOURCE CONVERTERS (VSC)

A voltage-source converter is a power electronic gadget, which can produce a sinusoidal voltage with any required extent, recurrence and stage point. Voltage source converters are generally utilized in flexible speed drives, yet can likewise be utilized to moderate voltage plunges. The VSC is utilized to either totally supplant the voltage or to infuse the 'missing voltage'. The 'missing voltage' is the distinction between the ostensible voltage and the real.

The converter is typically founded on some sort of vitality stockpiling, which will supply the converter with a DC voltage. The strong state gadgets in the converter is then changed to get the ideal yield voltage. Ordinarily the VSC isn't utilized for voltage plunge moderation, yet in addition for other power quality issues, for example gleam and music. The voltage source rectifier works by keeping the dc interface voltage at an ideal reference esteem, utilizing a criticism control circle as appeared in Figure 3 To achieve this errand, the dc interface voltage is estimated and contrasted and a reference V_{REF} . The mistake sign produced from this correlation is utilized to switch the six valves of the rectifier ON and OFF. Along these lines, power can come or come back to the air conditioner source as indicated by dc interface voltage necessities. Voltage V_D is estimated at capacitor C_D . At the point when the present I_D is sure (rectifier activity), the capacitor C_D is released, and the blunder sign approach the Control Block for more power from the air conditioner supply. The Control Block takes the power from the supply by producing the proper PWM signals for the six valves. Along these lines, increasingly current streams from the air conditioner to the dc side, and the capacitor voltage is recuperated. Conversely, when I_D winds up negative (inverter activity), the capacitor C_D is cheated, and the blunder sign requests that the control release the capacitor and return capacity to the air conditioner mains. The PWM control not exclusively can deal with the dynamic power, yet in addition receptive power, enabling this kind of rectifier to address power factor. Moreover, the air conditioner current waveforms can be kept up as practically sinusoidal, which lessens consonant defilement to the mains supply. Heartbeat width-regulation comprises of exchanging the valves ON and OFF, after a

pre-built up format. This layout could be a sinusoidal waveform of voltage or current. For instance, the tweak of one stage could be as the one appeared in Figure 4 This PWM example is a periodical waveform whose key is a voltage with a similar recurrence of the layout. The plentifulness of this key, called VMOD in Figure 4, is likewise relative to the abundance of the format. To make the rectifier work appropriately, the PWM example must produce a central VMOD with a similar recurrence as the power source.

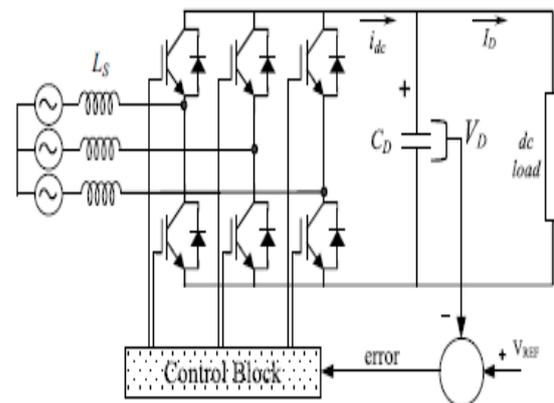


Figure 4: Operation principle of the voltage source rectifier.

Driving force factor rectifier, slacking force factor rectifier, driving force factor inverter, and slacking force factor inverter. Changing the example of tweak, as appeared in adjusts the extent of VMOD. Dislodging the PWM example changes the stage move. The communication among VMOD and V (source voltage) can be seen through a phasor chart. This connection licenses comprehension of the four-quadrant ability of this rectifier. In the accompanying tasks are shown:

- (a) rectifier at solidarity power factor;
- (b) inverter at solidarity power factor;
- (c) capacitor (zero power factor); and
- (d) inductor (zero power factor).

Is the rms estimation of the source current is. This present courses through the semiconductors similarly as appeared in Figure 4 Amid the positive half cycle, the transistor TN associated at the negative side of the dc connection is exchanged ON, and the current is starts to move through TN.

The present comes back to the mains and returns to the valves, shutting a circle with another stage, and going through a diode associated at a similar negative terminal of the dc connect. The current can likewise go to the DC load (reversal) and return through another transistor situated at the positive terminal of the dc interface. At the point when the transistor TN is turned OFF, the present way is interfered, and the present starts to move through diode DP, associated at the positive terminal of the dc connect. This current, called i_{Dp} in Fig, goes straightforwardly to the dc interface, helping in the age of the current i_{dc} . The current i_{dc} charges the capacitor CD and grants the rectifier to deliver dc control. The inductances LS are significant in this procedure, since they create a prompted voltage that permits conduction of the diode DP. A comparable task happens amid the negative half cycle, however with TP and DN.

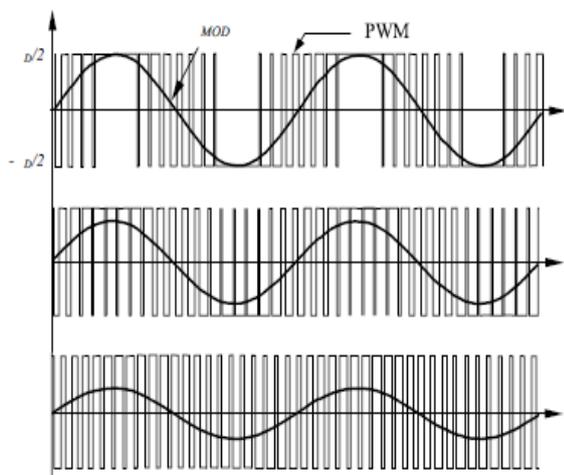


Figure 5: Changing V_{MOD} through the PWM pattern.

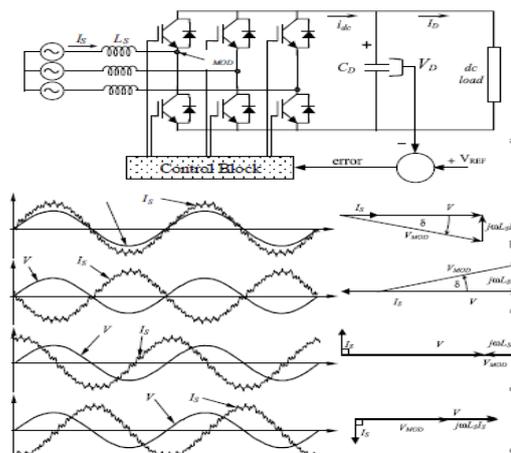


Figure 6 : Four-quadrant operation of the force-commutated rectifier: (a) the PWM force-commutated rectifier; (b) rectifier operation at unity power factor; (c) inverter operation at unity power factor; (d) capacitor operation at zero power factor; and (e) inductor operation at Zero power factor.

Under inverter task, the present ways are distinctive in light of the fact that the flows moving through the transistors come basically from the dc capacitor CD. Under rectifier activity, the circuit works like a Boost converter, and under inverter task it fills in as a Buck converter. To have full control of the activity of the rectifier, their six diodes must be enraptured contrarily at all estimations of immediate air conditioning voltage supply. Something else, the diodes will lead, and the PWM rectifier will carry on like a typical diode rectifier connect. The best approach to keep the diodes blocked is to guarantee a dc connect voltage higher than the pinnacle dc voltage produced by the diodes alone, as appeared in Figure 6 Along these lines, the diodes remain captivated contrarily, and they will lead just when in any event one transistor is exchanged ON, and great immediate air conditioning voltage conditions are given. V_D speaks to the capacitor dc voltage, which is kept higher than the typical diode-connect correction. To keep up this condition, the rectifier must have a control circle like the one showed.

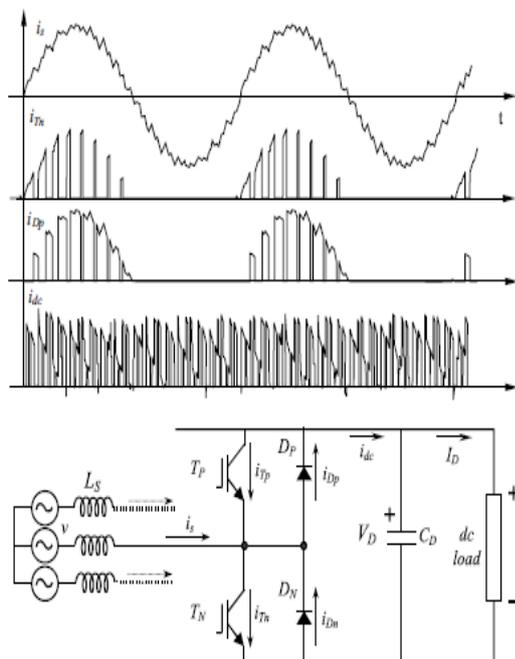


Figure 7 : Current waveforms through the mains, the valves, and the dc link.

V. THREE PHASE VOLTAGE SOURCE INVERTERS

Single-stage VSIs spread low-run control applications and three-stage VSIs spread the medium-to high-control applications. The primary motivation behind these topologies is to give a three-stage voltage source, where the plentifulness, stage, and recurrence of the voltages ought to dependably be controllable. Albeit the greater part of the applications require sinusoidal voltage waveforms (e.g., ASDs, UPSs, FACTS, var compensators), subjective voltages are additionally required in some rising applications (e.g., dynamic channels, voltage compensators). The standard three-stage VSI topology is appeared in Figure 8 furthermore, the eight substantial switch states are given As in single-stage VSIs, the switches of any leg of the inverter (S1 and S4, S3 and S6, or S5 and S2) can't be exchanged on at the same time since this would result in a short out over the dc interface voltage supply. Essentially, so as to stay away from vague

states in the VSI, and along these lines indistinct air conditioning yield line voltages, the switches of any leg of the inverter can't be turned off all the while as this will result in voltages that will rely on the separate line current extremity of the eight legitimate states, two of them produce zero air conditioning line voltages. For this situation, the air conditioner line flows freewheel through either the upper or lower parts. The rest of the states produce nonzero air conditioning yield voltages. So as to create a given voltage waveform, the inverter moves starting with one state then onto the next. Along these lines the subsequent air conditioning yield line voltages comprise of discrete estimations of voltages that are v_i , 0, and $\dot{y}v_i$ for the topology appeared in Figure 8 The choice of the states so as to create the given waveform is finished by the adjusting system that ought to guarantee the utilization of just the legitimate states.

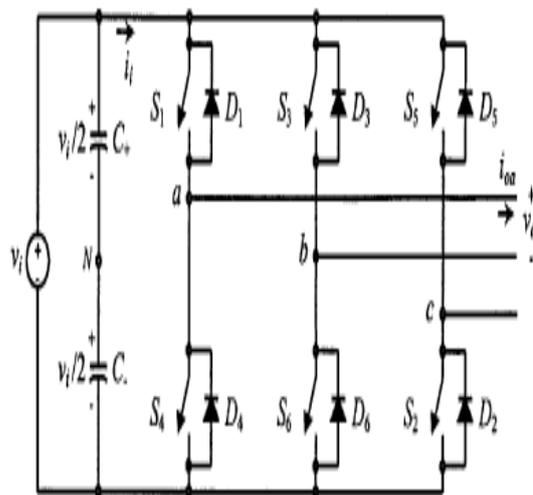


Figure 8: Circuit Diagram of Three-Phase Voltage Source Inverter

VI. TRANSFORMERS

A transformer is a gadget that exchanges electrical vitality starting with one circuit then onto the next through inductively coupled transmitters—the transformer's

curls. A changing current in the first or essential winding makes a differing attractive motion in the transformer's center and along these lines a fluctuating attractive field through the auxiliary winding. This fluctuating attractive field incites a changing electromotive power (EMF) or "voltage" in the auxiliary winding. This impact is called shared enlistment. In the event that a heap is associated with the auxiliary, an electric flow will stream in the optional winding and electrical vitality will be exchanged from the essential circuit through the transformer to the heap. In a perfect transformer, the actuated voltage in the optional winding (V_s) is in extent to the essential voltage (V_p), and is given by the proportion of the quantity of turns in the auxiliary (N_s) to the quantity of turns in the essential (N_p) as pursues. By suitable determination of the proportion of turns, a transformer consequently permits a rotating current (AC) voltage to be "ventured up" by making N_s more noteworthy than N_p , or "ventured down" by making N_s not as much as N_p . In by far most of transformers, the windings are curls twisted around a ferromagnetic center, air-center transformers being a striking special case. Transformers go in size from a thumbnail-sized coupling transformer covered up inside a phase mouthpiece to immense units gauging several tons used to interconnect bits of intensity networks. All work with a similar essential standards, despite the fact that the scope of plans is wide. While new innovations have disposed of the requirement for transformers in some electronic circuits, transformers are as yet found in almost all electronic gadgets intended for family unit ("mains") voltage. Transformers are basic for high voltage control transmission, which makes long separation transmission monetarily reasonable.

VII. PROPOSED CONTROL METHOD

7.1 The full state feedback scheme

The state feedback scheme includes feedback control, Feed forward control and decoupling control.

7.2 Feedback control

The feedback control is utilized to improve the preciseness of compensation voltage, the disturbance rejection capability and the robustness against parameter variations. As

in Figure 3, the capacitor voltage V_{cq}^e is the voltage control in the outer loop and the inductor current i_{mq}^e is the inner current control. The voltage control is implemented by a proportional regulator with voltage command V_{cq}^{e*} respectively produced by the voltage sag scheme.

7.3 Feed forward control

To improve the dynamic reaction of the voltage droop compensator, the feed forward control is added to the voltage control circle to remunerate the heap voltage promptly when voltage list happens. The feed forward voltage order is can be estimation by consolidating the remuneration voltage and the voltage drop over the channel inductor which is delivered by the channel capacitor current.

7.4 Decoupling control

Since cross coupling terms derived from the synchronous reference frame transformation and the external disturbances exists in the physical model of voltage sag compensator, the control block utilizes the decoupling control to improve the accuracy and the disturbance rejection ability. Figure 3 shows the decoupling terms is produced by measuring the load

current, filter capacitor voltage and the filter inductor current. The cross coupling terms in physical model can be eliminated completely.

VIII. INRUSH CURRENT MITIGATION TECHNIQUE

8.1 Flux Linkage DC Offset

The flux linkage is estimated by the measured line voltage. Figure 9 shows a single winding of the delta/bye three-phase load transformer which is installed in downstream of voltage sag compensator. The flux linkage of the phase a-b winding is expressed as

$$\lambda_{Lab}(t) = \int v_{Lab}(t) dt \quad (5)$$

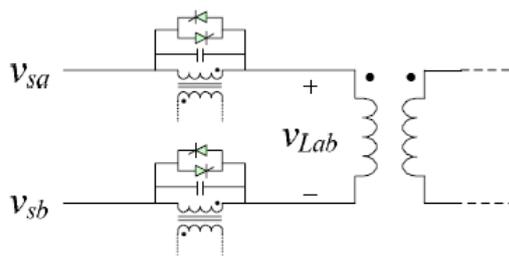


Figure 9: Transformer voltage and corresponding transient flux linkage

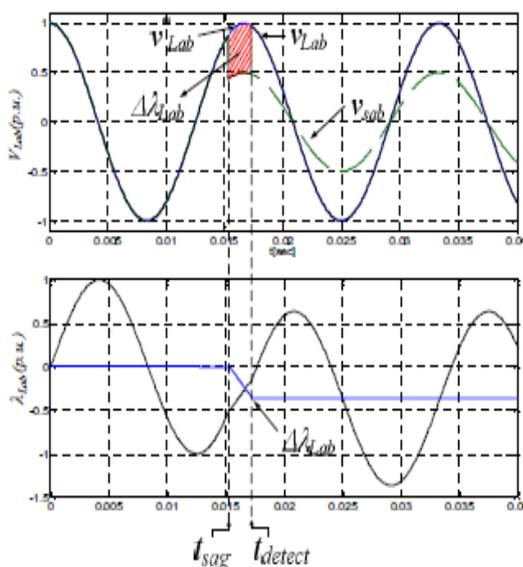


Figure 10: Connection diagram of the proposed system and delta/bye load transformer

Figure 10 illustrates the line-to-line voltage across the transformer winding and the resulting flux linkage from the sag occurrence to completion of voltage compensation. When voltage sags occurs ($t=t_{sag}$), the controller detects the sagged voltage and injects the required compensation voltage at $t=t_{detect}$. The flux linkage during the voltage compensation process can be express as following:

$$\lambda_{Lab}(t) = \lambda_{Lab}(t)|_{t=t_{sag}} + \int_{t_{sag}}^{t_{detect}} v_{Lab}(t) dt + \int_{t_{detect}}^t v_{Lab}^*(t) dt \quad (6)$$

This equation can be re-written as

$$\lambda_{Lab}(t) = \lambda_{Lab}(t)|_{t=t_{sag}} - \int_{t_{sag}}^{t_{detect}} v_{Lab}^*(t) dt + \int_{t_{sag}}^{t_{detect}} (v_{Lab}(t) - v_{Lab}^*(t)) dt + \int_{t_{detect}}^t v_{Lab}^*(t) dt \quad (7)$$

Assume the pre-fault load voltage is

$$v_{Lab}^*(t) = \hat{V}_{Lab}^* \sin(\omega t + \Phi_{Lab}^*)$$

Where \hat{V}_{Lab}^* the magnitude of load voltage, ω is the grid frequency, and Φ_{Lab}^* is the phase angle. Thus, after the voltage compensation is completed, the flux linkage can be expressed as

$$\lambda_{Lab}(t) = \Delta\lambda_{Lab}(t)|_{t=t_{detect}} + \frac{\hat{V}_{Lab}^*}{\omega} \sin(\omega t + \Phi_{Lab}^* - \frac{\pi}{2}) \quad (8)$$

Where

$$\Delta\lambda_{Lab}(t)|_{t=t_{detect}} = \lambda_{Lab}(t)|_{t=t_{sag}} - \lambda_{Lab}^*|_{t=t_{sag}} + \int_{t_{sag}}^{t_{detect}} (v_{Lab}(t) - v_{Lab}^*(t)) dt \quad (9)$$

for $t_{sag} \leq t < t_{detect}$

Equation (9) states that the sagged voltages cause the flux linkage DC offset $\Delta\lambda_{Lab}$ on the transformer windings, and its magnitude is dependent on the depth and the duration of sags. Severe voltage sag event can drive the DC offset exceeding the

magnetic saturation knee and causes high inrush current. In practical saturation, the magnetic saturation knee is usually put on 1.10-1.15 p.u. of state-study flux linkage.

IX. RESULTS

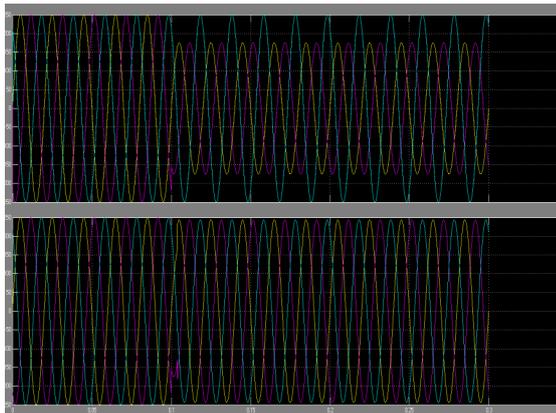


Figure 11: Source voltage and dvr voltage

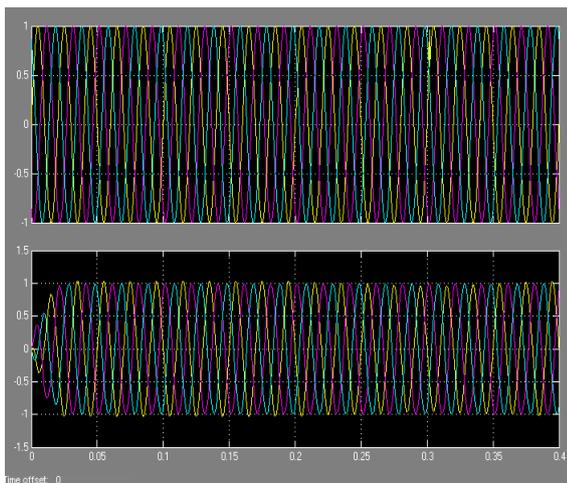


Figure 12 : Flux linkage of load transformer

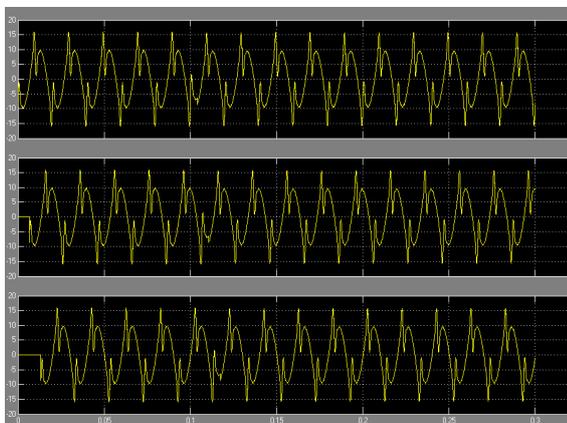


Figure 13 :Load current

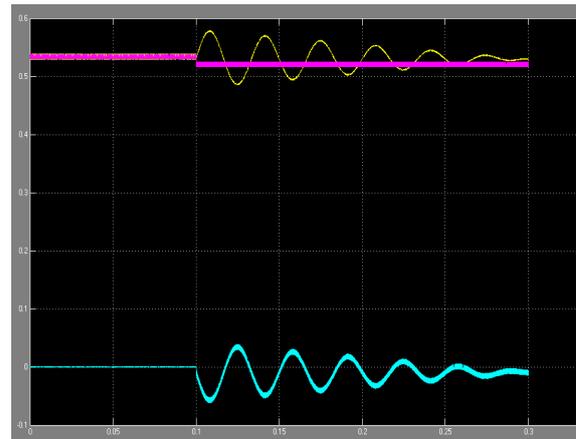


Figure 14 : Flux linkage of d-axis

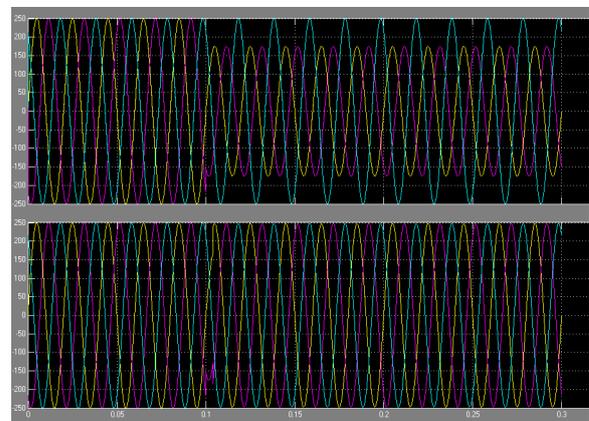


Figure 15 : Source voltage and load voltage

X. CONCLUSION

This task proposes an inrush current mitigation method consolidating with the full satisfy input controller to anticipate the inrush current during the voltage remuneration process. The controller incorporates a voltage control, a present control and a motion linkage control. The proposed control technique depends on the synchronous reference outline which empowers voltage hang compensator to accomplish quick voltage infusion and avert the inrush current. At the point when voltage hang happens, the controller can follow the transient motion linkage and compute a required pay voltage progressively for quick remuneration and disposal of transition linkage DC counterbalance brought about by voltage

droops. The viability of the proposed the transition linkage compensation mechanism is approved by research center test outcomes. It demonstrates that the proposed control technique gives a high unsettling influence dismissal capacity for voltage list compensator contrasted and regular voltage-current state criticism control strategy. The proposed strategy can be effectively incorporated with the current voltage hang pay control framework without utilizing any additional sensors.

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